

# **Transform Analysis of Linear Time-Invariant Systems**

## *Discrete-Time Signal Processing*

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# Introduction

- A linear time-invariant system is completely characterized by the impulse response  $h[n]$ .
- We can apply certain transforms to  $h[n]$ , such as the  $z$ -transform and the Fourier transform, and get equivalent representations.
- Looking at a system through these transforms is called **transform analysis**.

# Frequency Response

- The frequency response  $H(e^{j\omega})$  of a system is the eigenvalue for the input function  $e^{j\omega n}$ .
- The input/output signal's Fourier transforms are related by

$$Y(e^{j\omega}) = X(e^{j\omega}) H(e^{j\omega}).$$

- Thus, the magnitude and phase of input/output signals are related by

$$|Y(e^{j\omega})| = |X(e^{j\omega})| |H(e^{j\omega})|$$

$$\angle Y(e^{j\omega}) = \angle X(e^{j\omega}) + \angle H(e^{j\omega})$$

# Magnitude and Phase Response

- $|H(e^{j\omega})|$  is called the **magnitude response** or **gain**.
- $\angle H(e^{j\omega})$  is called the **phase response** or **phase shift**.
- Combined, they determine the system function,

$$H(e^{j\omega}) = |H(e^{j\omega})|e^{j\angle H(e^{j\omega})}.$$

- They are sometimes called **distortion**.

# Ideal Frequency Selective Filters

- The **ideal lowpass filter** is characterized by the frequency response

$$H_{lp}(e^{j\omega}) = \begin{cases} 1, & |\omega| < \omega_c \\ 0, & \omega_c < |\omega| \leq \pi \end{cases}$$

- The **ideal highpass filter** is characterized by the frequency response

$$H_{hp}(e^{j\omega}) = \begin{cases} 0, & |\omega| < \omega_c \\ 1, & \omega_c < |\omega| \leq \pi \end{cases}$$

# Magnitude and Phase

- Ideal lowpass filter

$$|H_{lp}(e^{j\omega})| = \begin{cases} 1, & |\omega| < \omega_c \\ 0, & \omega_c < |\omega| \leq \pi \end{cases}, \quad \angle H_{lp}(e^{j\omega}) = 0$$

- Similar for an ideal highpass filter.

# Ideal Delay System

- The impulse response is

$$h_{id}[n] = \delta[n - n_d].$$

- The frequency response is the Fourier transform

$$H_{id}(e^{j\omega}) = e^{-j\omega n_d},$$

so

$$|H_{id}(e^{j\omega})| = 1, \quad \angle H_{id}(e^{j\omega}) = -\omega n_d.$$

- The phase shift is linear in  $\omega$ . This is called a **linear-phase** property.

# Group Delay

- A measure of the linearity of the phase is the **group delay** defined by

$$\tau(\omega) = \text{grd}[H(e^{j\omega})] = -\frac{d}{d\omega} \{ \arg[H(e^{j\omega})] \}.$$

- Note here  $\arg[H(e^{j\omega})]$  is different from  $\angle H(e^{j\omega})$ . The former is defined to be a **continuous** function of  $\omega$ .
- An example of analysis is given in Figure 5.1 (system), 5.2 (input) and 5.3 (output).

# LCCDE Systems

- One thing about ideal frequency selective filter is that they cannot be implemented with finite computation.
- We need to consider a class of systems that are implementable.
- The class of causal systems characterized by linear constant-coefficient difference equations

$$\sum_{k=0}^N a_k y[n - k] = \sum_{k=0}^M b_k x[n - k]$$

is implementable, as the output can be computed recursively.

# $z$ -Domain Analysis

- Such a system (described by LCCDE) is best understood through the  $z$ -transform.
- Taking the  $z$ -transform,

$$\sum_{k=0}^N a_k z^{-k} Y(z) = \sum_{k=0}^M b_k z^{-k} X(z)$$
$$\Rightarrow H(z) = \frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^M b_k z^{-k}}{\sum_{k=0}^N a_k z^{-k}}$$

# General Properties of $H(z)$

- $H(z)$  is a ratio of polynomials in  $z^{-1}$ .
- It can be re-written as

$$H(z) = \left( \frac{b_0}{a_0} \right) \frac{\prod_{k=1}^M (1 - c_k z^{-1})}{\prod_{k=1}^N (1 - d_k z^{-1})}$$

- $(1 - c_k z^{-1})$  contributes a zero at  $z = c_k$  and a pole at  $z = 0$
- $(1 - d_k z^{-1})$  contributes a pole at  $z = d_k$  and a zero at  $z = 0$

# Example

- Consider the system function

$$H(z) = \frac{(1 + z^{-1})^2}{(1 - \frac{1}{2}z^{-1})(1 + \frac{3}{4}z^{-1})}$$

- Where are the poles and zeros?
- Can you implement this system?

# Region of Convergence

- Given a linear difference equation, we can always compute the functional form of  $H(z)$ .
- However, we cannot decide the **region of convergence**, thus failing to decide  $h[n]$ .
- The ambiguity can be resolved if further assumptions regarding **stability** and **causality** are given.

# Stability and Causality

- Specifically, for a system to be **stable**, the region of convergence must include the unit circle.
- In addition, for a system to be **causal**, the region of convergence must extend to  $\infty$ .
- It follows that if a system is causal and stable, *the outmost pole must be inside the unit circle.*

# Example

- Consider the LCCDE

$$y[n] - \frac{5}{2}y[n-1] + y[n-2] = x[n].$$

- The system function is

$$H(z) = \frac{1}{(1 - \frac{1}{2}z^{-1})(1 - 2z^{-1})}.$$

- Where are the poles?
- When is the system causal? stable? stable and causal? neither stable nor causal?

# Inverse Systems

- The inverse system  $H_i(z)$  of a system  $H(z)$  is defined to be the system that if it is cascaded with  $H(z)$ , the overall system is unity.
- That is,

$$H_i(z)H(z) = 1 \Rightarrow H_i(z) = \frac{1}{H(z)}.$$

- Equivalently

$$h_i[n] * h[n] = \delta[n].$$

# Inverse for LCCDE Systems

- Suppose we have an LCCDE system

$$H(z) = \left( \frac{b_0}{a_0} \right) \frac{\prod_{k=1}^M (1 - c_k z^{-1})}{\prod_{k=1}^N (1 - d_k z^{-1})}$$

- The inverse has a function form

$$H_i(z) = \left( \frac{a_0}{b_0} \right) \frac{\prod_{k=1}^N (1 - d_k z^{-1})}{\prod_{k=1}^M (1 - c_k z^{-1})}$$

- The poles of  $H(z)$  are the zeros of  $H_i(z)$  and vice versa.

# Does an Inverse Exist?

- Does an inverse exist for a given system with known  $H(z)$  and ROC?
- A necessary condition for an inverse system is that the ROC of  $H_i(z)$  must overlap with the ROC of  $H(z)$ .
- This condition helps to choose the ROC given the functional form of  $H_i(z)$ .

# Example

- Consider the system

$$H(z) = \frac{1 - 0.5z^{-1}}{1 - 0.9z^{-1}}, \text{ ROC } |z| > 0.9.$$

The pole is 0.9 and the zero is 0.5.

- The inverse system has a system function of

$$H_i(z) = \frac{1 - 0.9z^{-1}}{1 - 0.5z^{-1}}, \text{ ROC } |z| > 0.5,$$

where ROC is decided such that it overlaps with  $|z| > 0.9$ .

# Another Example

- Consider the system

$$H(z) = \frac{z^{-1} - 0.5}{1 - 0.9z^{-1}}, \text{ ROC } |z| > 0.9.$$

The pole is 0.9 and the zero is 2.

- The inverse system has a system function of

$$H_i(z) = \frac{1 - 0.9z^{-1}}{z^{-1} - 0.5} = \frac{-2 + 1.8z^{-1}}{1 - 2z^{-1}}.$$

Now both  $|z| > 2$  and  $|z| < 2$  overlaps with  $|z| > 0.9$ , so we have a choice.

# Causal and Stable Inverse

- Suppose a system with system function  $H(z)$  has zeros  $c_k$ 's and poles  $d_k$ 's. If it is causal and stable,

$$\max_k |d_k| < 1.$$

- An inverse system has poles  $c_k$ 's. For it to be causal and stable,

$$\max_k |c_k| < 1.$$

- *A causal and stable system has a causal and stable inverse system if and only if all poles and zeros are inside the unit circle.*

# Rational Causal System Function

- Any rational function of  $z^{-1}$  with only first-order poles can be written as

$$H(z) = \sum_{r=0}^{M-N} B_r z^{-r} + \sum_{k=1}^N \frac{A_k}{1 - d_k z^{-1}}.$$

- Assume the system is causal, the impulse response is

$$h[n] = \sum_{r=0}^{M-N} B_r \delta[n - r] + \sum_{k=1}^N A_k d_k^n u[n].$$

# IIR and FIR Systems

- If the system has any poles other than  $z = 0$ , then  $A_k \neq 0$  for some  $k$  and  $h[n]$  is not of finite length.
- The system is called a **infinite impulse response (IIR)** system.
- Otherwise,  $A_k = 0$  for all  $k$  and  $h[n]$  is of finite duration. Such a system is called **finite impulse response (FIR)**.
- Specifically, an FIR system has  $N = 0$  and

$$H(z) = \sum_{k=0}^M b_k z^{-k}.$$

# Example

- Consider the LCCDE

$$y[n] - ay[n - 1] = x[n].$$

- The system function is

$$H(z) = \frac{1}{1 - az^{-1}}.$$

- It is IIR.

# Frequency Response

- Suppose a causal LCCDE system is stable.
- The frequency response is the system function evaluated on the unit circle

$$H(e^{j\omega}) = \frac{\sum_{k=0}^M b_k e^{-j\omega k}}{\sum_{k=0}^N a_k e^{-j\omega k}}$$

- We are interested in the **magnitude, phase and group delay** of such a system.

# Magnitude Response

- The equation can be re-written as

$$H(e^{j\omega}) = \left( \frac{b_0}{a_0} \right) \frac{\prod_{k=1}^M (1 - c_k e^{-j\omega})}{\prod_{k=1}^N (1 - d_k e^{-j\omega})}$$

- So the magnitude response is

$$|H(e^{j\omega})| = \left| \frac{b_0}{a_0} \right| \frac{\prod_{k=1}^M |1 - c_k e^{-j\omega}|}{\prod_{k=1}^N |1 - d_k e^{-j\omega}|}$$

# Gain and Attenuation

- It is common practice to measure the magnitude in **decibels (dB)**, which is defined by

$$\text{Gain in dB} = 20 \log_{10} |H(e^{j\omega})|.$$

- When the gain  $|H(e^{j\omega})| < 1$ , we speak of **attenuation** in dB, which is defined by

$$\text{Attenuation in dB} = -20 \log_{10} |H(e^{j\omega})|.$$

# Gain, Phase and Delay

- For a causal stable LCCDE system,

$$\log_{10} |H(e^{j\omega})| = \log_{10} \left| \frac{b_0}{a_0} \right| + \sum_{k=1}^M \log_{10} |1 - c_k e^{-j\omega}| - \sum_{k=1}^N \log_{10} |1 - d_k e^{-j\omega}|.$$

- The phase response is

$$\angle H(e^{j\omega}) = \angle \left( \frac{b_0}{a_0} \right) + \sum_{k=1}^M \angle(1 - c_k e^{-j\omega}) - \sum_{k=1}^N \angle(1 - d_k e^{-j\omega})$$

- Similar for the group delay.
- Note that poles and zeros contribute to the sum similarly. Only the signs are opposite.

# A Single Zero

- Magnitude, phase, and group delay are sums of terms related to a zero or a pole.
- We now look at such a term. Suppose we have a zero at

$$z_0 = re^{j\theta}.$$

- The squared magnitude is

$$|1 - re^{j\theta}e^{-j\omega}|^2 = (1 - re^{j\theta}e^{-j\omega})(1 - re^{-j\theta}e^{j\omega}) = 1 + r^2 - 2r \cos(\omega - \theta).$$

- This is a periodic function of  $\omega$ , with period  $2\pi$ .

# Example

- The maximum occurs at  $\omega - \theta = \pi$ , while the minimum occurs at  $\omega - \theta = 0$ .
- For example, for  $r = 0.9$ , the maximum value gain in dB is

$$20 \log_{10}(1 + 0.9) = 5.57,$$

and the minimum is

$$20 \log_{10}(1 - 0.9) = -20.$$

- Varying  $\theta$  simply shifts the function.

# Phase and Group Delay

- The phase of such a term is

$$\text{ARG} [1 - r e^{j\theta} e^{-j\omega}] = \arctan \left[ \frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)} \right]$$

- The group delay is (need some basic calculus here, exercise)

$$\text{grd} [1 - r e^{j\theta} e^{-j\omega}] = \frac{r^2 - r \cos(\omega - \theta)}{1 + r^2 - 2r \cos(\omega - \theta)}$$

# Geometric Construction

- Again, we look at a first-order system

$$H(z) = (1 - re^{j\theta}z^{-1}) = \frac{z - re^{j\theta}}{z}.$$

- The magnitude response is

$$\left| \frac{e^{j\omega} - re^{j\theta}}{e^{j\omega}} \right| = \frac{|\nu_3|}{|\nu_1|} = |\nu_3|.$$

- $\nu_3$ , a vector from a zero to the unit circle, is called a **zero vector**.
- $\nu_1$ , a vector from a pole to the unit circle, is called a **pole vector**.

# Geometric Construction

- The corresponding phase is

$$\angle(1 - re^{j\theta}e^{-j\omega}) = \angle\nu_3 - \angle\nu_1 = \angle\nu_3 - \omega.$$

- We should now have a more concrete idea about the variation of magnitude and phase with respect to  $\omega$ , from the zero-pole plot of  $H(z)$ .

# Examples

- Figure 5.11 plots the frequency response for  $\theta = \pi$  and  $r = 1, 0.9, 0.7,$  and  $0.5$ .
- For the magnitude, it is maximum when  $\omega - \theta = \pi$  and minimum when  $\omega - \theta = 0$ , agreeing with (a).
- For the phase, the increase of  $\angle \nu_3$  is smaller than  $\angle \nu_1$  when  $0 \leq \omega \leq \pi/2$ , and is larger when  $\omega \sim \theta$ , agreeing with (b).
- For the group delay,  $\angle \nu_3$  increases fastest at  $\omega \sim \theta$ , agreeing with (c).

# More Examples

- Figure 5.13 plots the frequency response for  $\theta = \pi$  and  $r = 1/0.9, 1.25, \text{ and } 2.0$ . The zero is outside the unit circle.
- The magnitude follows a pattern similar to Figure 5.11.
- For the phase, the increase of  $\angle \nu_3$  is smaller than  $\angle \nu_1$  when  $0 \leq \omega \leq \pi/2$ . In contrast to Figure 5.13,  $\angle \nu_3$  actually decrease at  $\omega \sim \theta$ , leading to (b). Note there is a jump from  $-\pi$  to  $\pi$  at  $\omega = \theta$ .
- The group delay is always positive.

# Second-Order System

- Consider a system with complex conjugate pole,

$$H(z) = \frac{1}{(1 - re^{j\theta}z^{-1})(1 - re^{-j\theta}z^{-1})}$$

- The magnitude, phase and group delay are

$$- 10 \log_{10}[1 + r^2 - 2r \cos(\omega - \theta)] - 10 \log_{10}[1 + r^2 - 2r \cos(\omega + \theta)],$$

$$- \arctan \left[ \frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)} \right] - \arctan \left[ \frac{r \sin(\omega + \theta)}{1 - r \cos(\omega + \theta)} \right],$$

$$- \frac{r^2 - r \cos(\omega - \theta)}{1 + r^2 - 2r \cos(\omega - \theta)} - \frac{r^2 - r \cos(\omega + \theta)}{1 + r^2 - 2r \cos(\omega + \theta)}.$$

- Plots are given in Figure 5.16.

# Magnitude and Phase

- In general, the magnitude response and phase response of a system are independent.
- For an LCCDE system, there is some constraint between them.
- Under a condition referred to as **minimum phase**, the magnitude completely determines the phase and vice versa.

# Given Magnitude Response

- Suppose only the magnitude response is given for a system. That is, we have

$$|H(e^{j\omega})|^2 = H(e^{j\omega})H^*(e^{j\omega}) = H(z)H^*(1/z^*)|_{z=e^{j\omega}}.$$

- For a causal system characterized by LCCDE,

$$H(z) = \left(\frac{b_0}{a_0}\right) \frac{\prod_{k=1}^M (1 - c_k z^{-1})}{\prod_{k=1}^N (1 - d_k z^{-1})}, \quad H^*\left(\frac{1}{z^*}\right) = \left(\frac{b_0}{a_0}\right) \frac{\prod_{k=1}^M (1 - c_k^* z)}{\prod_{k=1}^N (1 - d_k^* z)}.$$

- What is the choice of the system function  $H(z)$ ?

# $C(z)$

- $|H(e^{j\omega})|^2$  is the following function evaluated at the unit circle

$$C(z) = H(z)H^*(1/z^*) = \left(\frac{b_0}{a_0}\right)^2 \frac{\prod_{k=1}^M (1 - c_k z^{-1})(1 - c_k^* z)}{\prod_{k=1}^N (1 - d_k z^{-1})(1 - d_k^* z)}$$

- For each pole  $d_k$  of  $H(z)$ , there is a pole of  $C(z)$  at  $d_k$  and  $(d_k^*)^{-1}$ .
- For each zero  $c_k$  of  $H(z)$ , there is a zero of  $C(z)$  at  $c_k$  and  $(c_k^*)^{-1}$ .
- $C(z)$  can be obtained by replacing  $e^{j\omega}$  by  $z$  in  $|H(e^{j\omega})|^2$ .

# Poles and Zeros

- The poles of  $C(z)$  occur in conjugate reciprocal pairs, i.e., pairs of  $d_k$  and  $(d_k^*)^{-1}$ .
  - If one is inside the unit circle, the other is outside.
  - Or they coincide on the unit circle.
- Similarly for the zeros.
- Suppose we have a causal, stable system. Then we know all the poles are inside the unit circle. There are no restriction for the zeros.
- Example 5.11 gives two distinct causal systems with the same  $C(z)$ .

# Poles and Zeros

- If we further assume that  $a_k, b_k$  are real numbers, then the poles and zeros of  $H(z)$  must occur in conjugate pairs or are on the real axis.
- Using this result in Example 5.12, there are still 4 choices for  $H(z)$  making the system causal and stable.
- If the number of zeros and poles are not limited, the number of causal and stable systems would also be unlimited.

# All-Pass System

- Consider a system function of the form

$$H_{ap}(z) = \frac{z^{-1} - a^*}{1 - az^{-1}}.$$

- On the unit circle,

$$|H_{ap}(e^{j\omega})| = \left| \frac{e^{-j\omega} - a^*}{1 - ae^{-j\omega}} \right| = |e^{-j\omega}| \left| \frac{1 - a^*e^{j\omega}}{1 - ae^{-j\omega}} \right| = 1,$$

since  $|e^{-j\omega}| = 1$  and  $1 - a^*e^{j\omega}$  is the complex conjugate of  $1 - ae^{-j\omega}$ .

- Such a system is called an **all-pass** system. Note if  $a$  is a pole,  $1/a^*$  is a zero.

# General All-Pass Systems

- For a general all-pass system with real impulse response, the system function can be written as

$$H_{ap}(z) = A \prod_{k=1}^{M_r} \frac{z^{-1} - d_k}{1 - d_k z^{-1}} \prod_{k=1}^{M_c} \frac{(z^{-1} - e_k^*)(z^{-1} - e_k)}{(1 - e_k z^{-1})(1 - e_k^* z^{-1})},$$

where  $d_k$  is a real pole, and  $(e_k, e_k^*)$  are a pair of conjugate poles.

- For causal and stable all-pass systems,  $|d_k| < 1$  and  $|e_k| < 1$ .
- The number of poles and zeros for such a system is

$$M = N = 2M_c + M_r.$$

# Phase Function

- For a first-order causal all-pass system, with  $a = re^{j\theta}$ ,  $r < 1$ , the phase function is

$$\begin{aligned}\angle \left( e^{-j\omega} \frac{1 - re^{j(\omega-\theta)}}{1 - re^{-j(\omega-\theta)}} \right) &= \angle e^{-j\omega} + \angle(1 - re^{j(\omega-\theta)}) - \angle(1 - re^{-j(\omega-\theta)}) \\ &= -\omega - 2 \arctan \left[ \frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)} \right].\end{aligned}$$

- For a second-order causal all-pass system, with poles at  $z = re^{\pm j\theta}$ , the phase function is the sum of two similar terms,

$$-2\omega - 2 \arctan \left[ \frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)} \right] - 2 \arctan \left[ \frac{r \sin(\omega + \theta)}{1 - r \cos(\omega + \theta)} \right].$$

# Phase Property

- The plots of Figure 5.22 and 5.23 are those of a first and second-order causal all-pass systems respectively.
- One can see that in the examples, the phases are non-positive for  $0 \leq \omega \leq \pi$ .
- The non-positiveness of phase is a general property of causal all-pass systems.

# Group Delay

- The group delay of a first-order causal all-pass system is

$$\text{grd} \left[ \frac{e^{-j\omega} - re^{-j\theta}}{1 - re^{j\theta}e^{-j\omega}} \right] = \frac{1 - r^2}{|1 - re^{j\theta}e^{-j\omega}|^2} > 0.$$

- For a general causal all-pass system with real impulse response,

$$\arg H(e^{j\omega}) = \arg \left( A \prod_{k=1}^{M_r} \frac{1 - d_k}{1 - d_k} \prod_{k=1}^{M_c} \frac{(1 - e_k^*)(1 - e_k)}{(1 - e_k)(1 - e_k^*)} \right) = 0.$$

- Thus the continuous phase  $\arg H(e^{j\omega})$  is non-positive.

# Minimum-Phase System

- Given  $C(z)$ , the square of magnitude response of a rational system,  $H(z)$  is not uniquely determined.
- We can require the system to be causal and stable, then the poles must be inside the unit circle. Still the system is not unique.
- If we further require the inverse system to be causal and stable, then the zeros must be inside the unit circle. Now the system is unique.
- The **minimum-phase system** is defined to be such a system.

# Decomposition

- Suppose  $H(z)$  has all zeros and poles are inside the unit circle except a zero at  $z = 1/c^*$ . Re-write

$$H(z) = H'(z)(z^{-1} - c^*) = H'(z)(1 - cz^{-1})\frac{z^{-1} - c^*}{1 - cz^{-1}}$$

- $H'(z)(1 - cz^{-1})$  has all the poles and zeros inside the unit circle, thus it is minimum-phase.
  - $(z^{-1} - c^*)/(1 - cz^{-1})$  is causal all-pass.
- By induction, we conclude that any rational system function can be written as

$$H(z) = H_{min}(z)H_{ap}(z).$$

# Example

- Consider the system function

$$H(z) = \frac{1 + 3z^{-1}}{1 + \frac{1}{2}z^{-1}}.$$

- The pole is inside the unit circle, but the zero is outside at  $z = -3$ .
- Identifying  $c = -\frac{1}{3}$ , we have

$$H(z) = H(z) \frac{1 + \frac{1}{3}z^{-1}}{1 + \frac{1}{3}z^{-1}} = 3 \left( \frac{1 + \frac{1}{3}z^{-1}}{1 + \frac{1}{2}z^{-1}} \right) \left( \frac{z^{-1} + \frac{1}{3}}{1 + \frac{1}{3}z^{-1}} \right) = H_{min}(z)H_{ap}(z).$$

# Second-Order Example

- Consider the system function

$$H(z) = \frac{(1 + \frac{3}{2}e^{j\pi/4}z^{-1})(1 + \frac{3}{2}e^{-j\pi/4}z^{-1})}{1 - \frac{1}{3}z^{-1}}.$$

- The pole is inside the unit circle, but the zeros are outside at  $z = -\frac{3}{2}e^{\pm j\pi/4}$ .
- Moving the zeros one by one, we have

$$\begin{aligned} H(z) &= H(z) \frac{1 + \frac{2}{3}e^{j\pi/4}z^{-1}}{1 + \frac{2}{3}e^{j\pi/4}z^{-1}} \frac{1 + \frac{2}{3}e^{-j\pi/4}z^{-1}}{1 + \frac{2}{3}e^{-j\pi/4}z^{-1}} \\ &= \frac{(1 + \frac{2}{3}e^{j\pi/4}z^{-1})(1 + \frac{2}{3}e^{-j\pi/4}z^{-1})}{1 - \frac{1}{3}z^{-1}} \frac{(1 + \frac{3}{2}e^{j\pi/4}z^{-1})(1 + \frac{3}{2}e^{-j\pi/4}z^{-1})}{(1 + \frac{2}{3}e^{j\pi/4}z^{-1})(1 + \frac{2}{3}e^{-j\pi/4}z^{-1})}. \end{aligned}$$

# Properties

- **The minimum phase-lag property**

$$H(z) = H_{min}(z)H_{ap}(z) \Rightarrow \arg H(e^{j\omega}) = \arg H_{min}(e^{j\omega}) + \arg H_{ap}(e^{j\omega})$$

The property follows since a stable and causal all-pass system has negative phase.

- **The minimum group-delay property**

$$\text{grd}[H(e^{j\omega})] = \text{grd}[H_{min}(e^{j\omega})] + \text{grd}[H_{ap}(e^{j\omega})]$$

The property follows since the group delay of a stable and causal all-pass system is positive.

# Linear-Phase Systems

- By definition, a linear-phase system has a frequency response of the following form

$$H(e^{j\omega}) = |H(e^{j\omega})|e^{-j\omega\alpha}.$$

- The phase, and group delay are

$$\angle H(e^{j\omega}) = -\omega\alpha; \quad \text{grd}[H(e^{j\omega})] = \alpha.$$

# Ideal Delay System

- Consider the **ideal delay system**  $y[n] = x[n - \alpha]$ . The frequency response is

$$H_{id}(e^{j\omega}) = e^{-j\omega\alpha}, \quad |\omega| < \pi.$$

- The magnitude, phase, and group delay are

$$|H_{id}(e^{j\omega})| = 1; \quad \angle H_{id}(e^{j\omega}) = -\omega\alpha; \quad \text{grd}[H_{id}(e^{j\omega})] = \alpha.$$

- This is an example of linear-phase systems, with constant magnitude.

# Generalized Linear-Phase Systems

- A generalized linear-phase system has a frequency response of the following form,

$$H(e^{j\omega}) = A(e^{j\omega}) e^{-j\omega\alpha + j\beta},$$

where  $\alpha, \beta$  are real constants and  $A(e^{j\omega})$  is a real function of  $\omega$ .

- Note that  $A(e^{j\omega})$  can be negative, so it is not strictly an amplitude.
- Ignoring any discontinuities, we have a constant group delay

$$\text{grd}[H(e^{j\omega})] = \alpha.$$

# Necessary Condition

- For a generalized linear-phase system, we have

$$\begin{aligned} H(e^{j\omega}) &= A(e^{j\omega}) e^{-j\omega\alpha + j\beta} \\ &= A(e^{j\omega}) \cos(\beta - \omega\alpha) + jA(e^{j\omega}) \sin(\beta - \omega\alpha) \\ &= \sum h[n] e^{-j\omega n} = \sum h[n] \cos \omega n - j \sum h[n] \sin \omega n \\ \Rightarrow \frac{\sin(\beta - \omega\alpha)}{\cos(\beta - \omega\alpha)} &= -\frac{\sum h[n] \sin \omega n}{\sum h[n] \cos \omega n} \\ \Rightarrow \sum h[n] (\cos(\beta - \omega\alpha) \sin \omega n + \sin(\beta - \omega\alpha) \cos \omega n) &= 0 \end{aligned}$$

- It follows that

$$\sum_n h[n] \sin[\omega(n - \alpha) + \beta] = 0 \text{ for all } \omega.$$

# Symmetric Cases

- In symmetric cases, we have  $h[M - n] = h[n]$  (symmetric with respect to the middle point  $\frac{M}{2}$ ).
- We have the flexibility to choose  $\alpha, \beta$ , but the necessary condition must be satisfied.
- Setting  $\beta = 0$  (or  $\pi$ ), and  $2\alpha$  to be an integer  $M$ , we have

$$\begin{aligned} \sum_n h[n] \sin[\omega(n - \alpha) + \beta] &= \sum_n h[n] \sin[\omega(n - \alpha)] \\ &= \left( \sum_{n=-\infty}^{\lfloor \frac{M-1}{2} \rfloor} + \sum_{n=\lfloor \frac{M-1}{2} \rfloor + 1}^{\lceil \frac{M+1}{2} \rceil - 1} + \sum_{n=\lceil \frac{M+1}{2} \rceil}^{\infty} \right) h[n] \sin[\omega(n - \alpha)] \\ &= \sum_{n=-\infty}^{\lfloor \frac{M-1}{2} \rfloor} (h[n] - h[M - n]) \sin[\omega(n - \alpha)] = 0. \end{aligned}$$

# Anti-Symmetric Cases

- In anti-symmetric cases, we have  $h[M - n] = -h[n]$  (anti-symmetric with respect to the middle point  $\frac{M}{2}$ ).
- With the conditions  $\beta = \pi/2$ ,  $2\alpha = M$ , we have

$$\begin{aligned} \sum_n h[n] \sin[\omega(n - \alpha) + \beta] &= \sum_n h[n] \cos[\omega(n - \alpha)] \\ &= \left( \sum_{n=-\infty}^{\lfloor \frac{M-1}{2} \rfloor} + \sum_{n=\lfloor \frac{M-1}{2} \rfloor + 1}^{\lceil \frac{M+1}{2} \rceil - 1} + \sum_{n=\lceil \frac{M+1}{2} \rceil}^{\infty} \right) h[n] \cos[\omega(n - \alpha)] \\ &= \sum_{n=-\infty}^{\lfloor \frac{M-1}{2} \rfloor} (h[n] + h[M - n]) \cos[\omega(n - \alpha)] = 0. \end{aligned}$$

- Similarly for  $\beta = 3\pi/2$ .

# Causal GLP Systems

- If the system is causal,

$$\sum_{n=0}^{\infty} h[n] \sin[\omega(n - \alpha) + \beta] = 0 \text{ for all } \omega.$$

- Furthermore, the condition of symmetry and anti-symmetry implies that

$$h[n] = 0, \quad n < 0 \text{ or } n > M.$$

- So it is FIR.

# Type I Systems

- A type I system is defined by

$$h[n] = \begin{cases} h[M - n], & 0 \leq n \leq M \\ 0, & \text{otherwise,} \end{cases} \quad M \text{ is even.}$$

- The frequency response is

$$H(e^{j\omega}) = \left( \sum_{k=0}^{M/2} a[k] \cos \omega k \right) e^{-j\omega M/2},$$

where

$$a[0] = h[M/2], \quad a[k] = 2h[M/2 - k].$$

# Frequency Response

- Let  $\alpha = M/2$ .

$$\begin{aligned} H(e^{j\omega}) &= \sum_{n=0}^M h[n]e^{-j\omega n} = \left( \sum_{n=0}^{\alpha-1} + \sum_{n=\alpha+1}^M \right) h[n]e^{-j\omega n} + h[\alpha]e^{-j\omega\alpha} \\ &= \sum_{k=1}^{\alpha} \left( h[\alpha - k]e^{-j\omega(\alpha-k)} + h[\alpha + k]e^{-j\omega(\alpha+k)} \right) + h[\alpha]e^{-j\omega\alpha} \\ &= \sum_{k=1}^{\alpha} h[\alpha - k] \left( e^{-j\omega(\alpha-k)} + e^{-j\omega(\alpha+k)} \right) + h[\alpha]e^{-j\omega\alpha} \\ &= \sum_{k=1}^{\alpha} h[\alpha - k]e^{-j\omega\alpha} \left( e^{j\omega k} + e^{-j\omega k} \right) + h[\alpha]e^{-j\omega\alpha} \\ &= \left( \sum_{k=0}^{\alpha} a[k] \cos \omega k \right) e^{-j\omega\alpha} \end{aligned}$$

# Type II Systems

- A type II system is defined by

$$h[n] = \begin{cases} h[M - n], & 0 \leq n \leq M \\ 0, & \text{otherwise,} \end{cases} \quad M \text{ is odd.}$$

- The frequency response is

$$H(e^{j\omega}) = \left( \sum_{k=1}^{(M+1)/2} b[k] \cos \left[ \omega \left( k - \frac{1}{2} \right) \right] \right) e^{-j\omega M/2},$$

where

$$b[k] = 2h[(M + 1)/2 - k].$$

# Frequency Response

- Let  $\alpha = M/2$ .

$$\begin{aligned} H(e^{j\omega}) &= \sum_{n=0}^M h[n]e^{-j\omega n} = \left( \sum_{n=0}^{\alpha-1/2} + \sum_{n=\alpha+1/2}^M \right) h[n]e^{-j\omega n} \\ &= \sum_{k=1}^{\alpha+1/2} \left( h\left[\alpha + \frac{1}{2} - k\right]e^{-j\omega\left(\alpha + \frac{1}{2} - k\right)} + h\left[\alpha - \frac{1}{2} + k\right]e^{-j\omega\left(\alpha - \frac{1}{2} + k\right)} \right) \\ &= \sum_{k=1}^{\alpha+1/2} h\left[\alpha + \frac{1}{2} - k\right] \left( e^{-j\omega\left(\alpha + \frac{1}{2} - k\right)} + e^{-j\omega\left(\alpha - \frac{1}{2} + k\right)} \right) \\ &= \sum_{k=1}^{\alpha+1/2} h\left[\alpha + \frac{1}{2} - k\right]e^{-j\omega\alpha} \left( e^{j\omega\left(k - \frac{1}{2}\right)} + e^{-j\omega\left(k - \frac{1}{2}\right)} \right) \\ &= e^{-j\omega M/2} \sum_{k=1}^{\alpha+1/2} 2h\left[\alpha + \frac{1}{2} - k\right] \cos \left[ \omega\left(k - \frac{1}{2}\right) \right] \end{aligned}$$

# Type III Systems

- A type III system is defined by

$$h[n] = \begin{cases} -h[M - n], & 0 \leq n \leq M \\ 0, & \text{otherwise,} \end{cases} \quad M \text{ is even.}$$

- The frequency response is

$$H(e^{j\omega}) = j \left( \sum_{k=1}^{M/2} c[k] \sin \omega k \right) e^{-j\omega M/2},$$

where

$$c[k] = 2h[M/2 - k].$$

# Frequency Response

- Let  $\alpha = M/2$ .  $h[\alpha] = 0$  by definition.

$$\begin{aligned} H(e^{j\omega}) &= \sum_{n=0}^M h[n]e^{-j\omega n} = \left( \sum_{n=0}^{\alpha-1} + \sum_{n=\alpha+1}^M \right) h[n]e^{-j\omega n} \\ &= \sum_{k=1}^{\alpha} \left( h[\alpha - k]e^{-j\omega(\alpha-k)} + h[\alpha + k]e^{-j\omega(\alpha+k)} \right) \\ &= \sum_{k=1}^{\alpha} h[\alpha - k] \left( e^{-j\omega(\alpha-k)} - e^{-j\omega(\alpha+k)} \right) \\ &= \sum_{k=1}^{\alpha} h[\alpha - k]e^{-j\omega\alpha} \left( e^{j\omega k} - e^{-j\omega k} \right) \\ &= je^{-j\omega\alpha} \left( \sum_{k=1}^{\alpha} c[k] \sin \omega k \right) \end{aligned}$$

# Type IV Systems

- A type IV system is defined by

$$h[n] = \begin{cases} -h[M - n], & 0 \leq n \leq M \\ 0, & \text{otherwise,} \end{cases} \quad M \text{ is dd.}$$

- The frequency response is

$$H(e^{j\omega}) = j \left( \sum_{k=1}^{(M+1)/2} d[k] \sin \left[ \omega \left( k - \frac{1}{2} \right) \right] \right) e^{-j\omega M/2},$$

where

$$d[k] = 2h[(M + 1)/2 - k].$$

# Frequency Response

- Let  $\alpha = M/2$ .

$$\begin{aligned} H(e^{j\omega}) &= \sum_{n=0}^M h[n]e^{-j\omega n} = \left( \sum_{n=0}^{\alpha-1/2} + \sum_{n=\alpha+1/2}^M \right) h[n]e^{-j\omega n} \\ &= \sum_{k=1}^{\alpha+1/2} \left( h\left[\alpha + \frac{1}{2} - k\right]e^{-j\omega\left(\alpha + \frac{1}{2} - k\right)} + h\left[\alpha - \frac{1}{2} + k\right]e^{-j\omega\left(\alpha - \frac{1}{2} + k\right)} \right) \\ &= \sum_{k=1}^{\alpha+1/2} h\left[\alpha + \frac{1}{2} - k\right] \left( e^{-j\omega\left(\alpha + \frac{1}{2} - k\right)} - e^{-j\omega\left(\alpha - \frac{1}{2} + k\right)} \right) \\ &= \sum_{k=1}^{\alpha+1/2} h\left[\alpha + \frac{1}{2} - k\right]e^{-j\omega\alpha} \left( e^{j\omega\left(k - \frac{1}{2}\right)} - e^{-j\omega\left(k - \frac{1}{2}\right)} \right) \\ &= je^{-j\omega M/2} \sum_{k=1}^{\alpha+1/2} 2h\left[\alpha + \frac{1}{2} - k\right] \sin[\omega(k - 1/2)] \end{aligned}$$

# Example

- Figure 5.36 gives FIR linear-phase systems of each type.
- The frequency responses are given in Examples 5.17-5.20.

$$\left\{ \begin{array}{l} H_{\text{I}}(e^{j\omega}) = e^{-j\omega 2} \frac{\sin(5\omega/2)}{\sin(\omega/2)}, \quad (M = 4) \\ H_{\text{II}}(e^{j\omega}) = e^{-j\omega 5/2} \frac{\sin(3\omega)}{\sin(\omega/2)}, \quad (M = 5) \\ H_{\text{III}}(e^{j\omega}) = j[2 \sin(\omega)]e^{-j\omega}, \quad (M = 2) \\ H_{\text{IV}}(e^{j\omega}) = j[2 \sin(\omega/2)]e^{-j\omega/2}, \quad (M = 1) \end{array} \right.$$

# System Function

- Consider the system function of an FIR linear-phase system

$$H(z) = \sum_{n=0}^M h[n]z^{-n}.$$

- For either the symmetric or the anti-symmetric cases,

$$H(z) = \sum_{n=0}^M \pm h[M-n]z^{-n} = \sum_{k=0}^M \pm h[k]z^k z^{-M} = \pm z^{-M} H(z^{-1}).$$

- It follows that if  $z_0$  is a zero, so is  $z_0^{-1}$ , since

$$H(z_0^{-1}) = z_0^M H(z_0) = 0.$$

# Location of Zeros

- If  $h[n]$  is real, the zeros come in complex conjugate pairs.
- Let  $z_0 = re^{j\theta}$  be a zero. From our discussion, we see that the quadruple

$$(re^{j\theta}, re^{-j\theta}, r^{-1}e^{j\theta}, r^{-1}e^{-j\theta})$$

are all zeros.

- $r = 1, \theta \neq 0, \pi$ , two zeros;
- $r \neq 1, \theta = 0, \pi$ , two zeros;
- $r = \pm 1$ , one zero;

# Symmetric/Anti-symmetric Cases

- For the symmetric cases (Types I and II),

$$H(z) = z^{-M} H(z^{-1}).$$

- $z = -1$  must be a zero for odd  $M$ .

- For the anti-symmetric cases (Types III and IV),

$$H(z) = -z^{-M} H(z^{-1}).$$

- $z = 1$  must be a zero.

- $z = -1$  must be a zero for even  $M$ .